

**KEYASK GENERATION PROJECT STAGE IV
STUDIES-PHYSICAL ENVIRONMENT
GN-9.1.1- EXISTING AND PROJECT ENVIRONMENT
FLOW FILES**
**Water Resources Engineering Department
Power Planning Division**



Oct. 1, 2012

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**KEYYASK GENERATION PROJECT
STAGE IV STUDIES - PHYSICAL ENVIRONMENT
EXISTING AND PROJECT ENVIRONMENT FLOW FILES**

REV 0

DELIVERABLE GN 9.1.1

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INTEROFFICE MEMORANDUM

From J. Malenchak, Ph.D., P.Eng Section Head Sediment and Ice Studies Water Resource Engineering Department Power Planning Division	TO M. E. St. Laurent, M.Sc., P.Eng. Section Head Nelson River Keeyask Project Hydro Power Planning Department Power Projects Development Division
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DATE 2012 09 01

FILE 00195-11100-00136_01

SUBJECT **KEYYASK GENERATING STATION – PHYSICAL ENVIRONMENT STUDIES**
EXISTING AND PROJECT ENVIRONMENT FLOW FILES
MEMORANDUM GN-9.1.1-REV 0

Please find the attached report “Keeyask Generation Project Stage IV Studies - Physical Environment: Existing and Project Environment Flow Files GN-9.1.1”. This report documents the development of existing and post-project flow files used in the Stage IV Engineering and Physical Environment Impact Statement studies.

This technical memorandum is to be used in support of the Keeyask Generating Station Environmental Impact Statement. In order to provide appropriate interpretation and guidance, please consult the Water Resource Engineering Department prior to external distribution.

Please contact me at (204) 360-5028 or JMalenchak@hydro.mb.ca if you have any questions or concerns.

Sincerely,

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1 SUMMARY

The Existing Environment inflow file for the Keeyask Generating Station (GS) Environmental Impact Statement (EIS) has been estimated. The Existing Environment inflow file is derived using Kettle GS total outflow discharge, change in storage on Stephens Lake, and local inflow between Kettle GS and Split Lake outlet on a daily time step. The geographic location of the Existing Environment inflow data is located at the Split Lake outlet, and the recommended time period for the existing inflow file is from September 1, 1977 to December 2006. The Post-Project flow file has been calculated with SPLASH modeling outputs. The Post-Project flow regime is based on four scenarios of SPLASH outputs using a time period from April 1912 to March 2006. Various duration curves for the existing environment and post-project flow data have been developed. Results show that the potential flow regime change under the Post-Project scenarios will be minor. With comparisons showing that the flow difference for all percentile values will be less than 10% with the exception of the 5 percentile flow in winter which will realize a difference of 12.2%.

2 BACKGROUND

Characterizing the flow regime at the proposed Keeyask GS for both Existing environment and Post-Project is required for the EIS. The proposed GS is located on the Nelson River at Gull Rapids immediately upstream of Stephens Lake (Figure 1). Inflow to the GS is governed by the outflow from Split Lake which is approximately 50 km upstream of the GS. Since no flow records are available at the site of Keeyask GS, inflow to the GS needs to be estimated.

Due to the close proximity to Split Lake, Keeyask inflows can be approximated by Split Lake outflows. In 1977, the Churchill River Diversion (CRD) was constructed, diverting water from the Churchill River into the Burntwood River and eventually into Split Lake. Since there is a noticeable discontinuity in Split Lake discharges after the CRD, only the recorded discharges from Split Lake after 1977 are used to characterize the existing environment.

In order to characterize possible flow regime changes after a new generating station is operational, the SPLASH model was developed by Manitoba Hydro to estimate Post-Project flows. The SPLASH model considers the entire Manitoba Hydro generation system. The model is able to simulate Post-Project flow considering long term inputs into the system and the incorporation of past and future generation components. The SPLASH outputs are flow file scenarios based in terms of a prediction of future electricity loads and generation capacity. In this study, four Post-project flow files at the Keeyask GS are calculated based on SPLASH outputs at the Lake Winnipeg outlet and Notigi Control on a monthly time step. The time period of the post project flow files is from April 1912 to March 2006. Since the model considers long term inputs into the system, this longer post-project flow file (when compared to the existing

environment flow file which had a marked discontinuity in 1977 due to the CRD) was considered to be more representative.

3 EXISTING ENVIRONMENT FLOW REGIME

3.1 LOCAL INFLOW ESTIMATION

In order to estimate daily inflows to the Keeyask GS for the existing environment, local inflows between the Split Lake outlet and the Kettle GS were first computed. This study uses the rational method for local inflow estimation. The Kettle River basin is selected as an index basin since it neighbors the local inflow basin between the Split Lake outlet and Kettle GS. The recorded daily discharge at hydrometric station (05UF004) on the Kettle River was extracted from the Water Survey of Environment Canada data sets. The area of the Kettle River basin and the local inflow sub-basin was computed using ArcGIS. The geographic location of the relevant sub-basins and generating stations are illustrated in Figure 1. Figure 2 shows the estimated daily local inflow hydrograph.

3.2 KEYASK GS INFLOW CALCULATION

In the hydraulic system between Split Lake Outlet and the Kettle GS, a mass conservation equation for a daily time step can be given by:

$$\frac{dS_{\text{Stephens}}}{dt} \approx \frac{\Delta S_{\text{Stephens}}}{\Delta t} = \frac{f(H + \Delta H) - f(H)}{\Delta t} = -Q_{\text{Kettle GS}} + Q_{\text{Local}} + Q_{\text{Keeyask GS}} \quad (1)$$

where

S_{Stephens} = Storage in Stephens Lake for a given day;

$\Delta S_{\text{Stephens}}$ = Storage change in Stephens Lake for a given day;

$f(H)$ = Stage-storage relation function;

ΔH = Daily water surface elevation change in Stephens Lake;

$Q_{\text{Kettle GS}}$ = Total daily outflow at the Kettle GS;

Q_{Local} = Daily local inflow between Split Lake outlet and Kettle GS;

$Q_{\text{Keeyask GS}}$ = Daily inflow to the Keeyask GS at the Split lake outlet;

Δt = 24 hours.

At the Kettle GS forebay, a stage-storage relationship equation is developed, graphically depicted in Figure 3. In reality, average water surface elevation changes on Stephens lake (ΔH) and the elevation changes measured at the Kettle GS forebay are often different since the flow at Stephens Lake can be unsteady varied flow. In order to use the storage-elevation equation depicted in Figure 3, equation (1) is transformed into:

$$\begin{aligned} Q_{\text{Keeyask GS}} &= Q_{\text{Kettle GS}} - Q_{\text{Local}} + \left(\frac{f(H_0 + \Delta H_0) - f(H_0)}{\Delta t} + \frac{\Delta S'}{\Delta t} \right) \\ &= \left(Q_{\text{Kettle GS}} - Q_{\text{Local}} + \frac{\Delta S}{\Delta t} \right) + \frac{\Delta S'}{\Delta t} = Q_{\text{cal}} + \Delta Q' \end{aligned} \quad (2)$$

where H_0 is water surface elevation at the Kettle GS forebay; ΔH_0 is water surface elevation change at the forebay; ΔS is storage change on Stephens Lake calculated by the equation shown in Figure 3; and $\Delta S'$ is the adjustment of storage change ΔS ; and $\Delta Q'$ is the relevant discharge adjustment corresponding to $\Delta S'$.

Since the values of $\Delta Q'$ are unknown, a practical way to estimate the value of $Q_{\text{Keeyask GS}}$ is to take multi-day moving average of the calculated values Q_{cal} . In this study, the multi-day moving average is taken using intervals that range from 2 to 8 days. Since an open water rating curve is developed at the Split Lake outlet, the following criterion is used to select the best existing environment flow file using the multi-day moving average values.

$$\text{Min } E! = \sqrt{\sum (q_i^{\text{Keeyask GS}} - q_i^{\text{Split Lake}})^2} \quad (3)$$

where $q_i^{\text{Keeyask GS}}$ is the Keeyask GS open water daily flow found using the multi-day moving average of $Q_{\text{Keeyask GS}}$; $q_i^{\text{Split Lake}}$ is Split lake outlet open water daily flow calculated using the rating curve; and the minimum value of $E!$ indicates the best estimate.

In the process of calculation, daily outflow discharge data at the Kettle GS and 24-hour end water level elevation on Stephens Lake were extracted from the Manitoba Hydro Daily Hydrometric Database. The open water rating curve at the Split Lake outlet shown in Figure 4 was referenced from “*Keeyask Generating Station Stage 4 Studies Updated Open Water Hydraulics Memorandum GN-2.1, Draft 2, April 21, 2005*” (Manitoba Hydro, 2004). The rating curve was used to generate the daily flow file ($q_i^{\text{Split Lake}}$) at the Split Lake outlet based on observed water level data.

It was found that the 7-day moving average daily flow file is the best estimate for the inflow to the Keeyask GS under existing environment conditions. As a result, the flow file by taking the 7-day moving average of the flow data calculated from equation (1) is used as the estimated inflow to the Keeyask GS. Figure 5 illustrates the estimated Keeyask GS daily flow hydrograph, and the corresponding monthly average flow hydrograph is shown in Figure 6.

3.3 EXISTING ENVIRONMENT FLOW DURATION CURVES

The estimated Keeyask GS daily inflow file was used to develop the existing environment duration curves. Figure 7 illustrates the daily flow duration curves for the existing environment, and the corresponding monthly average discharge duration curves are demonstrated in Figure 8. For reference purposes, open water season is defined as May 1 – Oct. 31 in this study and the winter season would therefore be defined as Nov. 1 – Apr. 30.

4 POST-PROJECT FLOW REGIME

4.1 POST-PROJECT FLOW FILES

According to the possible time schedule of building Conawapa and Keeyask GS and the projection of future electricity load of the entire system, four SPLASH Post-Project flow files are selected in this study. Each Post-Project file is based on a corresponding scenario of electricity load and generation capacity as follows:

- Existing_2008 (existing capacity with load year 2008)
- Conawapa_2023 (existing capacity plus Conawapa GS with load year 2023)
- Conawapa + Keeyask + IC_2023 (existing capacity plus Conawapa plus Keeyask plus Inter-Connection with load year 2023)
- Single Cycle Combustion Turbine (SCCT)_2023 (existing capacity plus SCCT with load year 2023)

It should be noted that the system load of 2023 could occur any time in the future. Since the SPLASH modeled monthly discharges are located at the Lake Winnipeg outlet and Notigi Control, the Post-Project inflows to the Keeyask GS under a given scenario were computed by adding them to the local inflows (inflow between Lake Winnipeg outlet/Notigi Control and the Split Lake outlet). Local inflows were calculated based on the methodology described in the long term streamflow data technical reports (Manitoba Hydro, 1990). Figure 9 demonstrates the computed Post-Project flow files at the Keeyask GS.

4.2 POST-PROJECT FLOW REGIME

The duration curve corresponding to each scenario of computed Post-Project flow file for the Keeyask GS was developed separately for all season, open water, and winter, as shown in Figures 10-12. The figures also illustrate the Post-Project mean flow duration curve which is developed by putting all-scenario flow data together. The graphs show both the variation among Post-project flow files and their deviation against the mean values.

For the Post-project flow files, a representative flow file from the four flow files needs to be selected in order to obtain the hydrograph to be used in the EIS. This study uses a least-square method to identify a representative Post-project flow file, which is chosen based on the maximum least-square value between the mean flow (all scenarios) duration curve values and each Post-project flow file duration curve values. The results show that the Conawapa+Keeyask+IC_2023 scenario has the most representative Post-project flow file. Table 1 lists the Post-project flow data of the representative scenario.

5 DISCUSSION AND CONCLUSIONS

Figures 13-15 show a comparison of the duration curves for the Existing Environment monthly flow data and the Conawapa+Keeyask+IC_2023 inflow file for all-season, open water, and winter, respectively. The comparison shows that the flow difference for different percentile values is small since the difference is less than 10% except when considering the 5 percentile flow in winter (12.2% difference). The difference between the two flow files is also associated with two different periods being used in Existing Environment (1977-2006) and Post-Project (1912-2006). Therefore, the potential flow regime change under the Post-Project environment will be minor. A comparison of the Existing Environment and Post-Project monthly flow data for identical time periods (1977-2006) can be found in Figure 16. The purpose of this illustration is to show that the SPLASH output compares well with existing environment measured data for the same time period.

6 GLOSSARY

<i>existing environment</i>	Refers to the environment in which a proposed generating station is to be built, under the conditions that exist prior to it actually being built.
<i>forebay</i>	A reservoir feeding the intake of a hydroelectric power plant.
<i>inflow</i>	Refers to flow discharge to a reservoir/lake/forebay.
<i>least-squares analysis</i>	A statistical procedure that determines the minimum value, among a set of alternatives, of the numerical difference between two series raised to the second power.
<i>outflow</i>	Refers to flow discharge from a reservoir/lake.
<i>post-project</i>	Refers to the environment in which a proposed generating station is to be built, under the conditions that exist after it has been built.
SPLASH	Manitoba Hydro's comprehensive long term resource planning analysis tool, which evaluates system-wide energy production and benefits of various system expansion options under current and future load scenarios.

7 REFERENCES

Manitoba Hydro (1990), Long Term Streamflow Data Phase II, Stage I: Streamflow Data Extension 1968 to 1988 Period. T. M. No. 90/4-1.

Manitoba Hydro (2005), Keeyask Generating Station Stage IV Studies Updated Open Water Hydraulics Memorandum GN-2.1, Rev 0.

8 APPENDIX A - ABBREVIATIONS

ABBREVIATIONS

cms..... cubic metres per second

CRD Churchill River Diversion

EIS environmental impact statement

GS..... generating station

IC inter-connection

km..... kilometre

m..... metre

SCCT single cycle combustion turbine

9 APPENDIX B - FIGURES AND TABLES

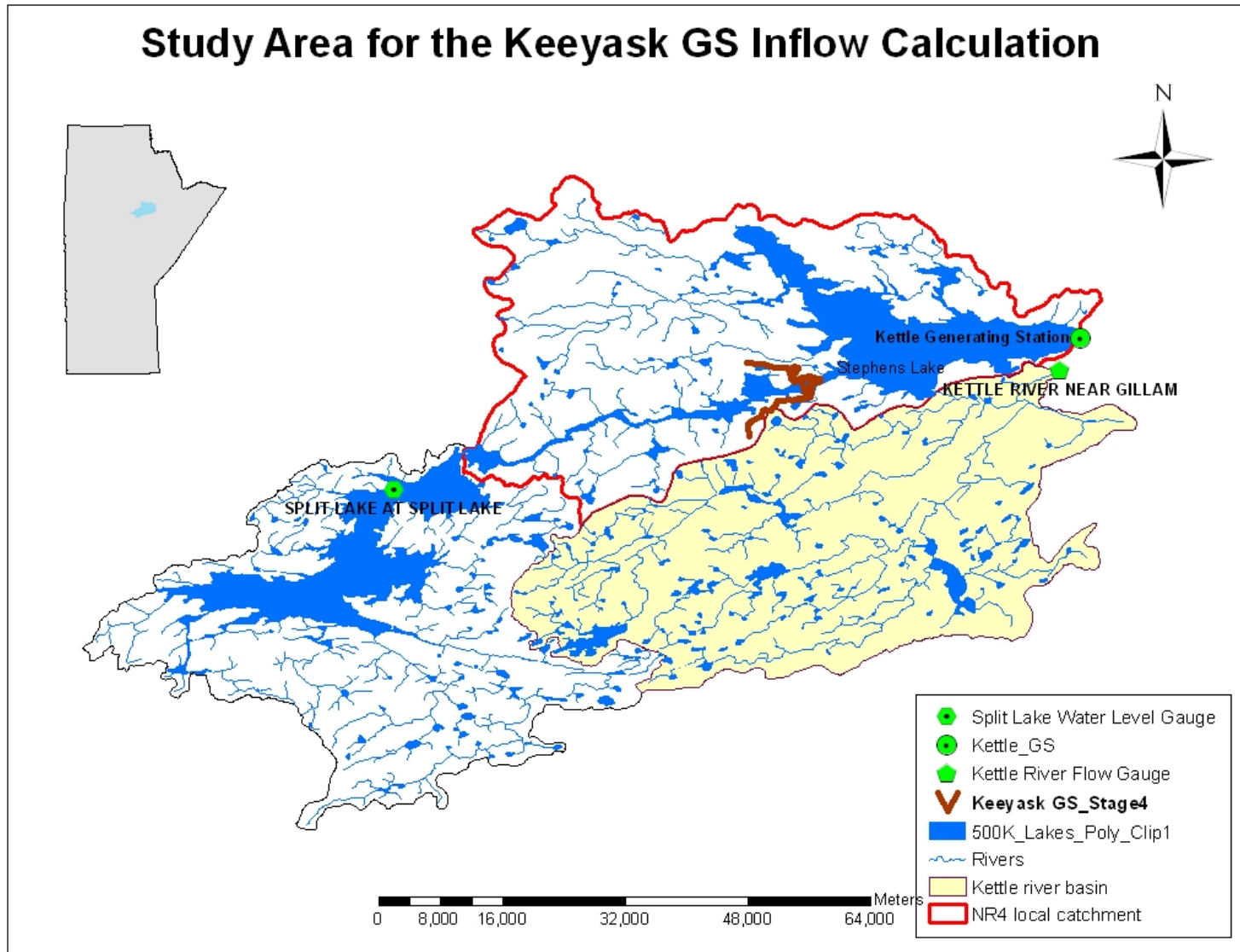


Figure 1 Study area

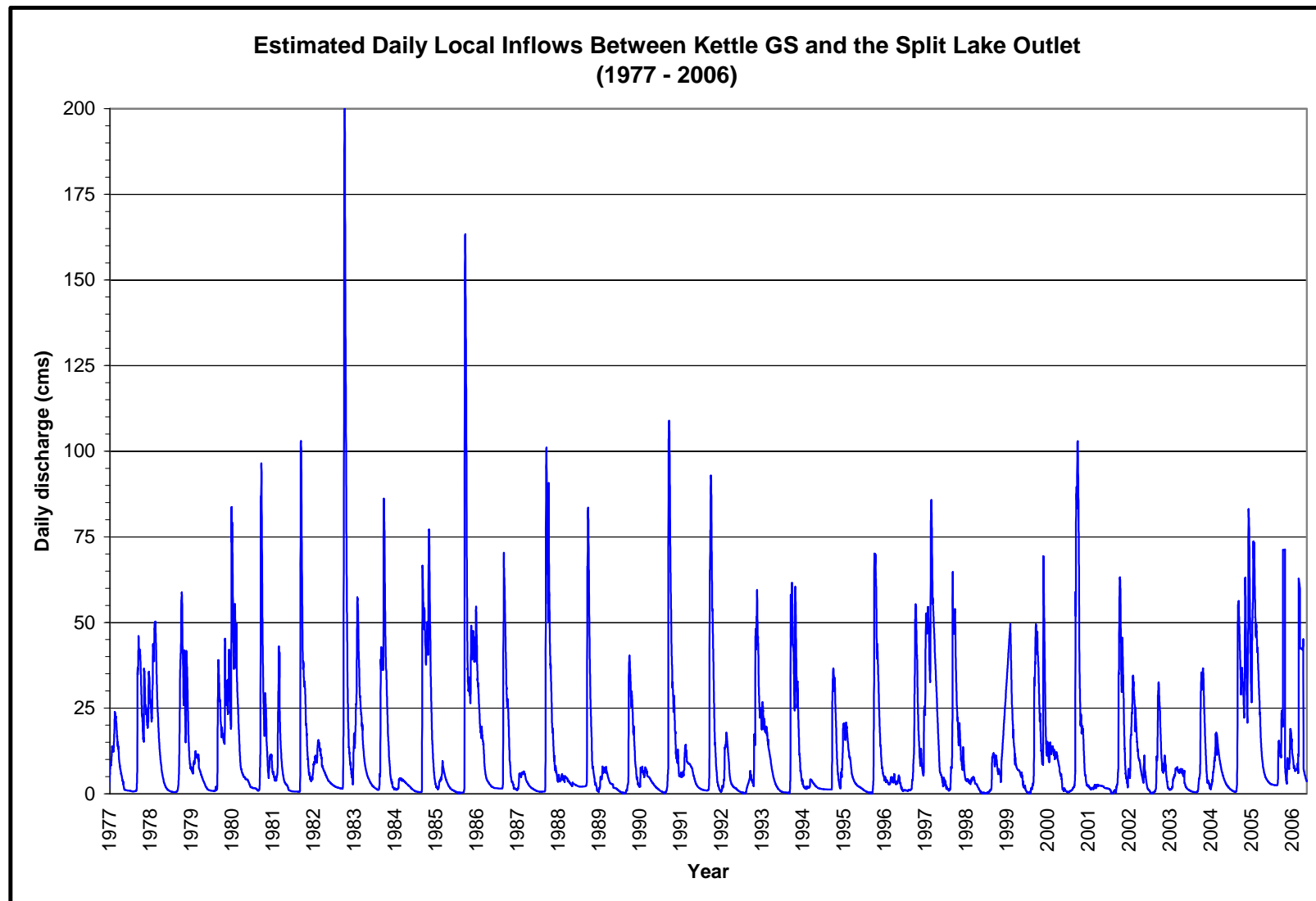


Figure 2 Estimated daily local inflow hydrograph (1977 – 2006)

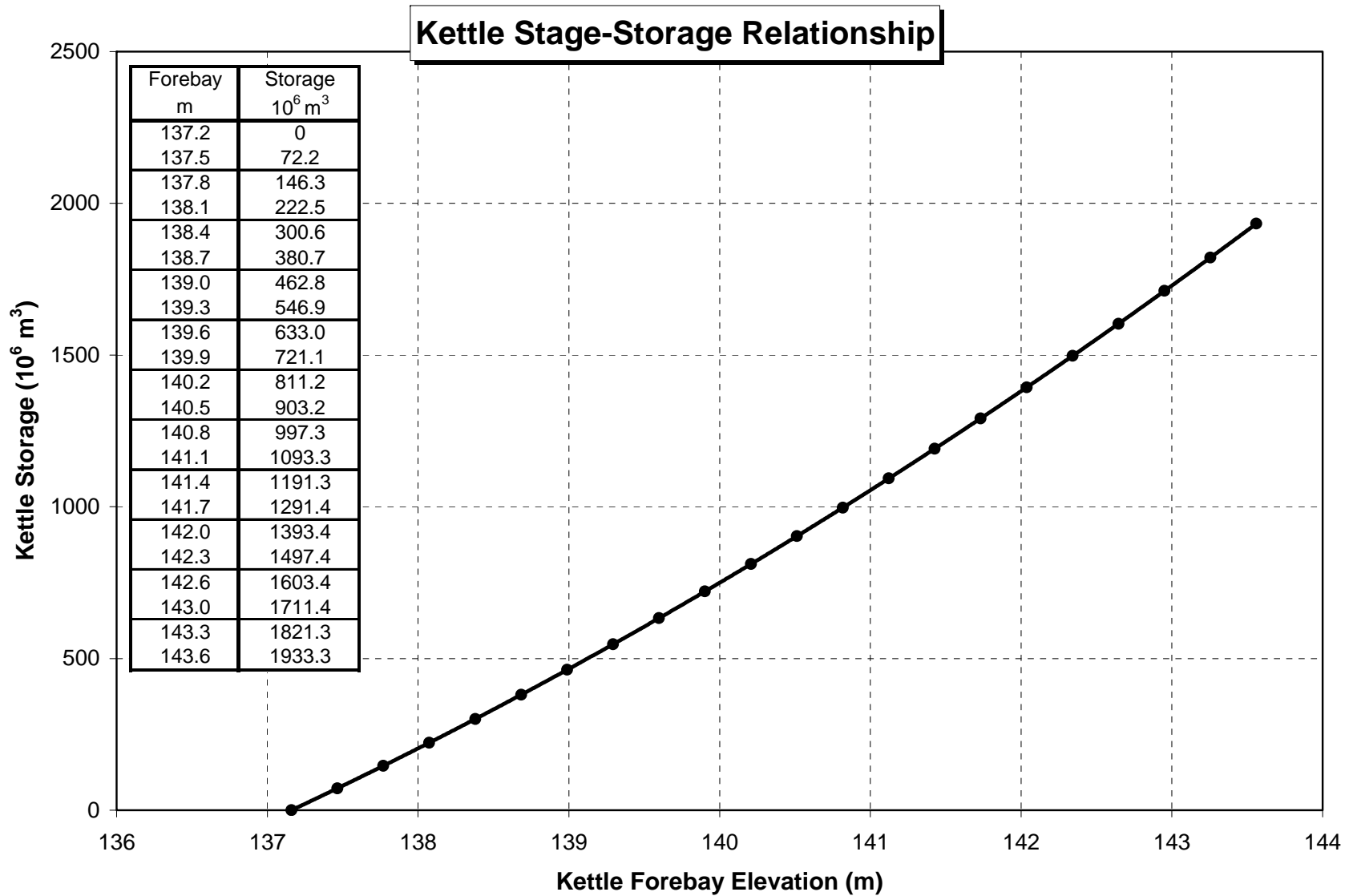


Figure 3 Stage-storage relationship at Stephens Lake (Kettle Forebay)

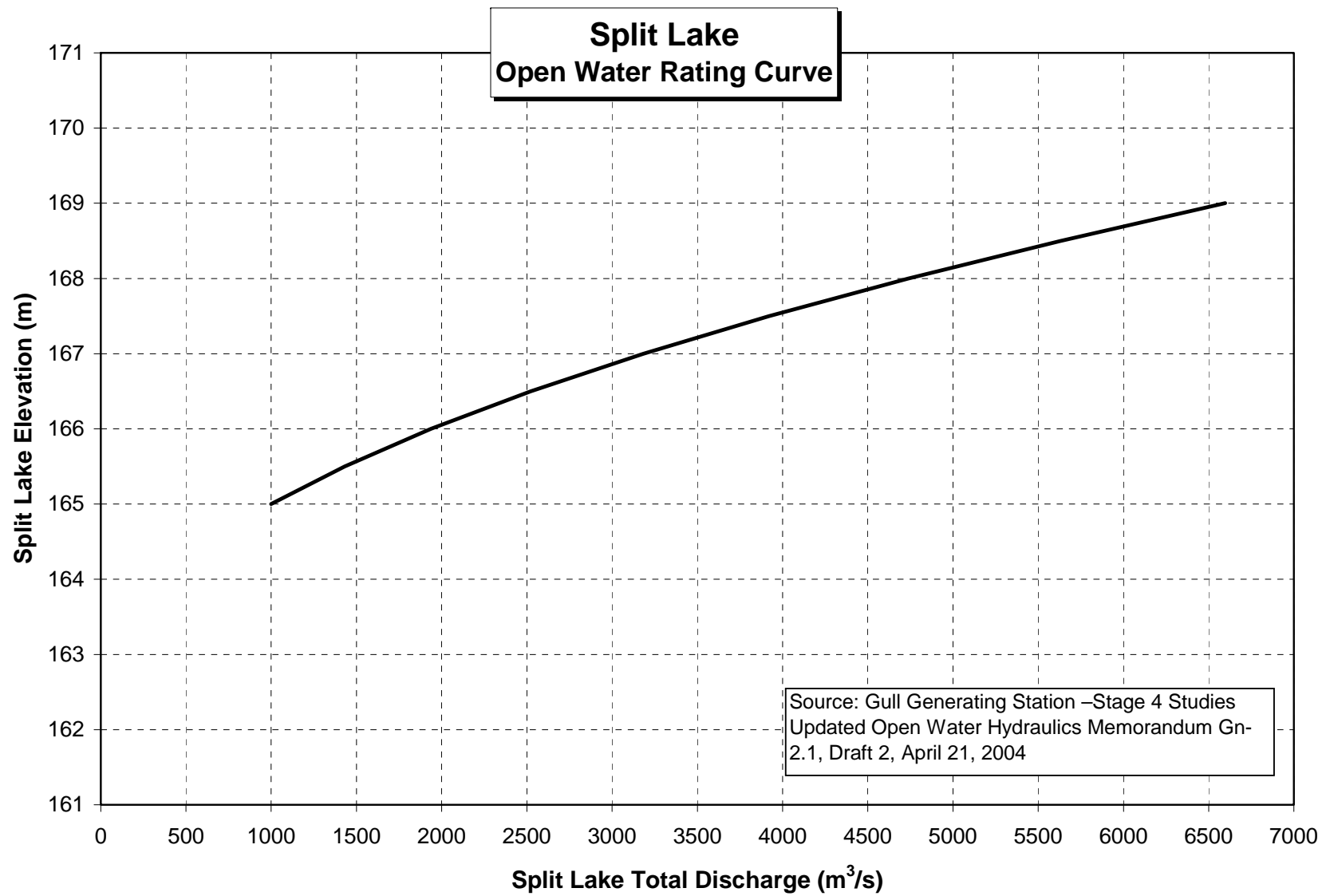


Figure 4 Split Lake open water rating curve

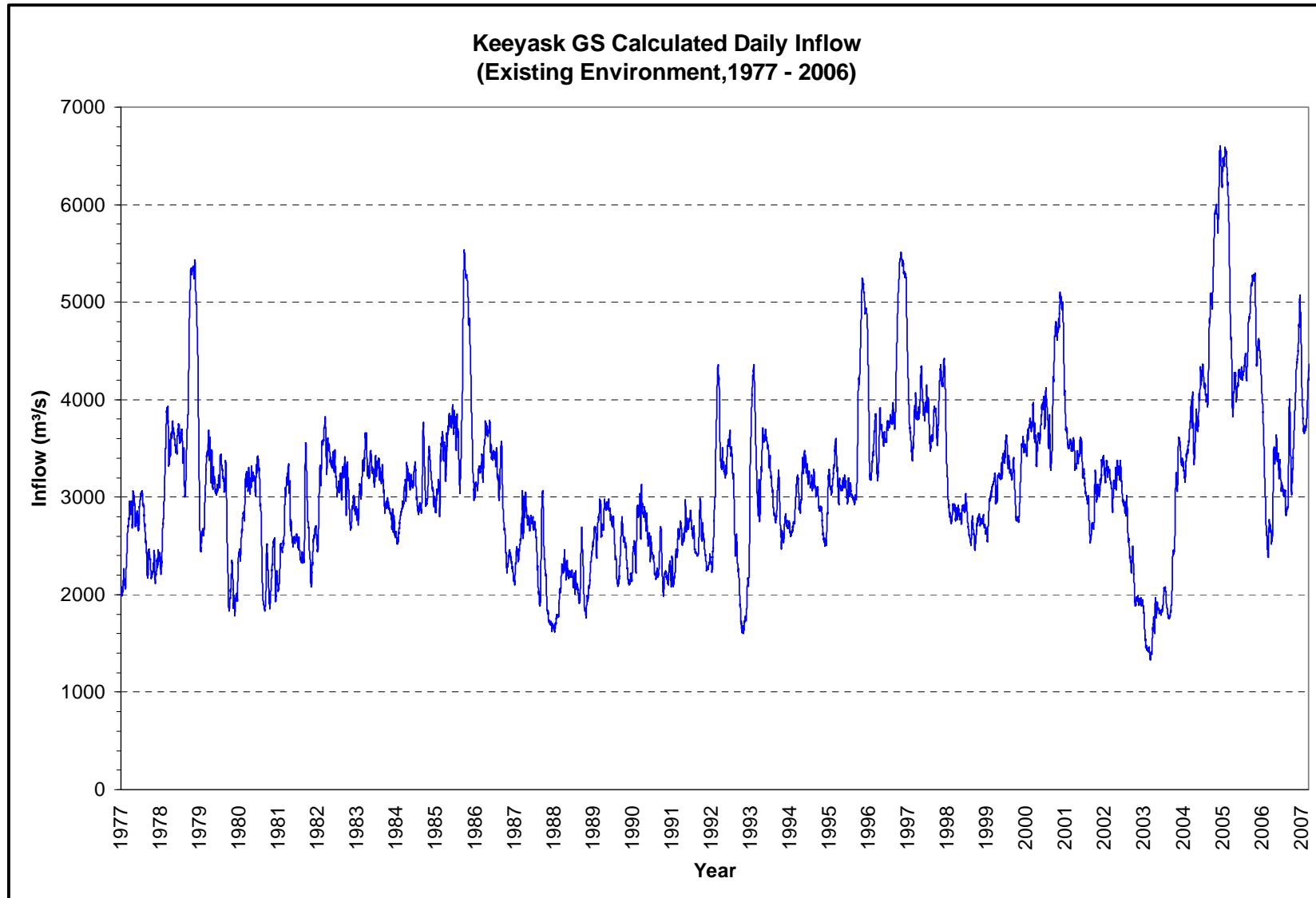


Figure 5 Keyask GS calculated daily inflow hydrograph (1977 – 2006)

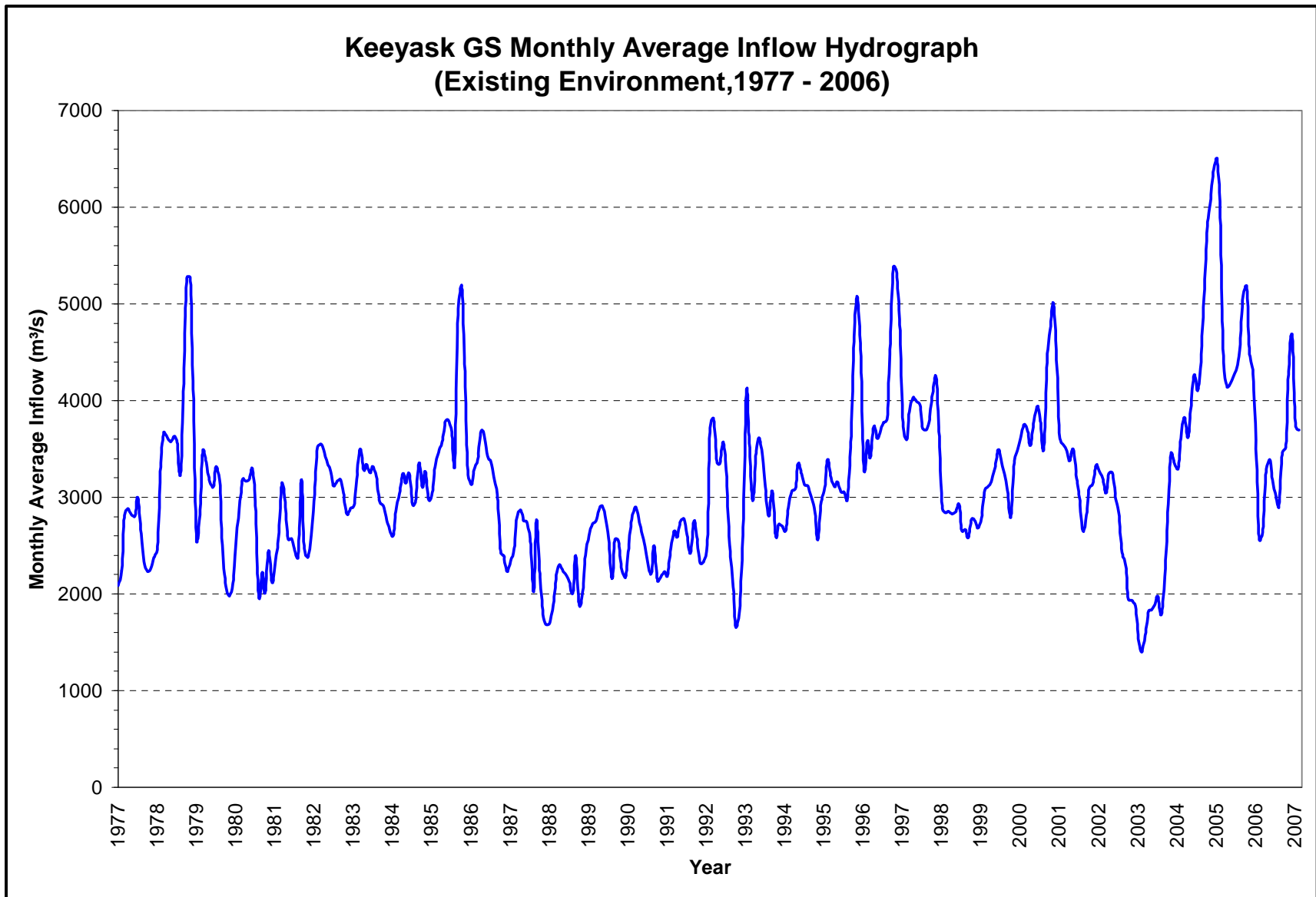


Figure 6 Keyask GS monthly average inflow hydrograph (1977 – 2006)

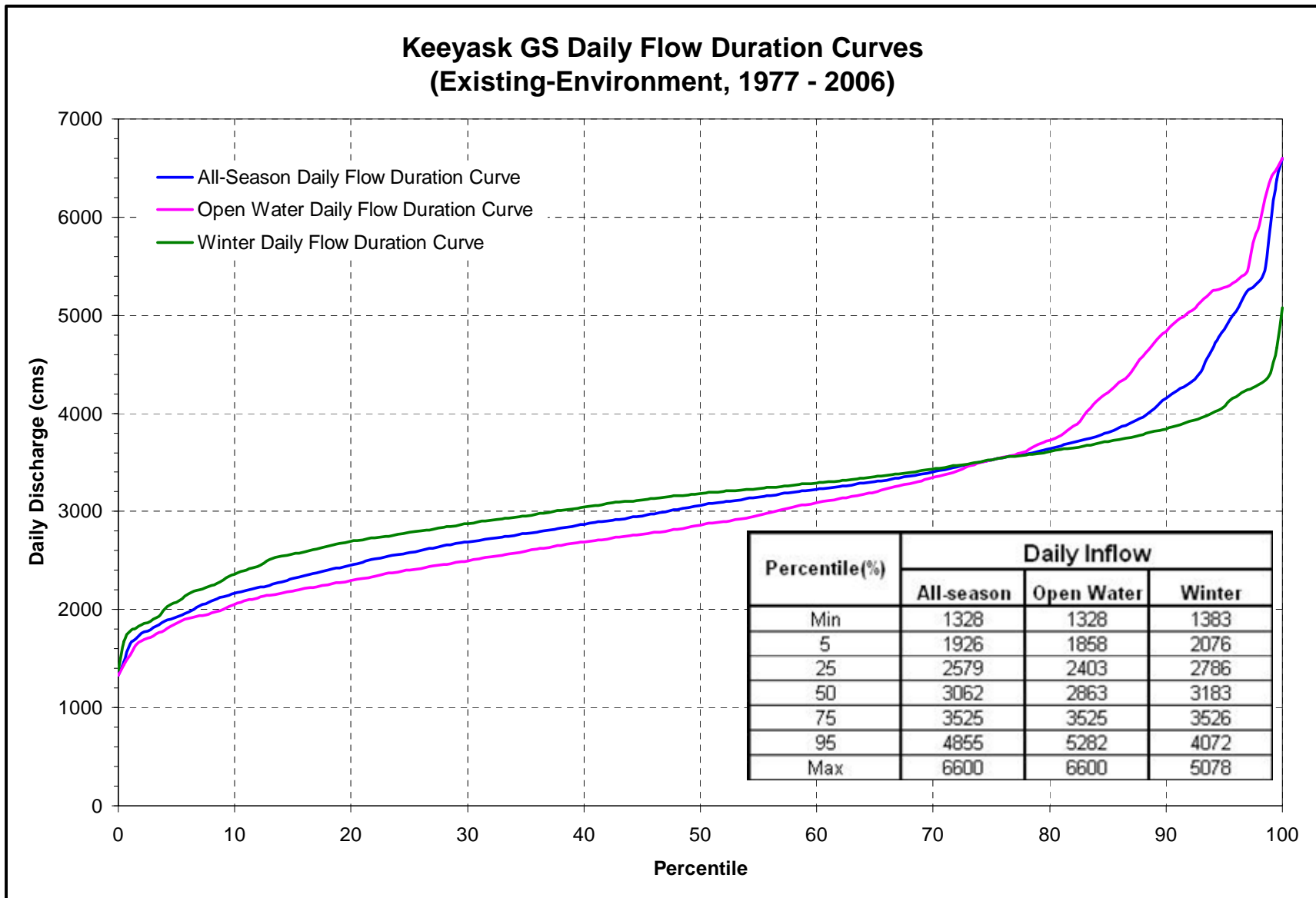


Figure 7 Keyask GS existing environment daily inflow duration curves (1977 – 2006)

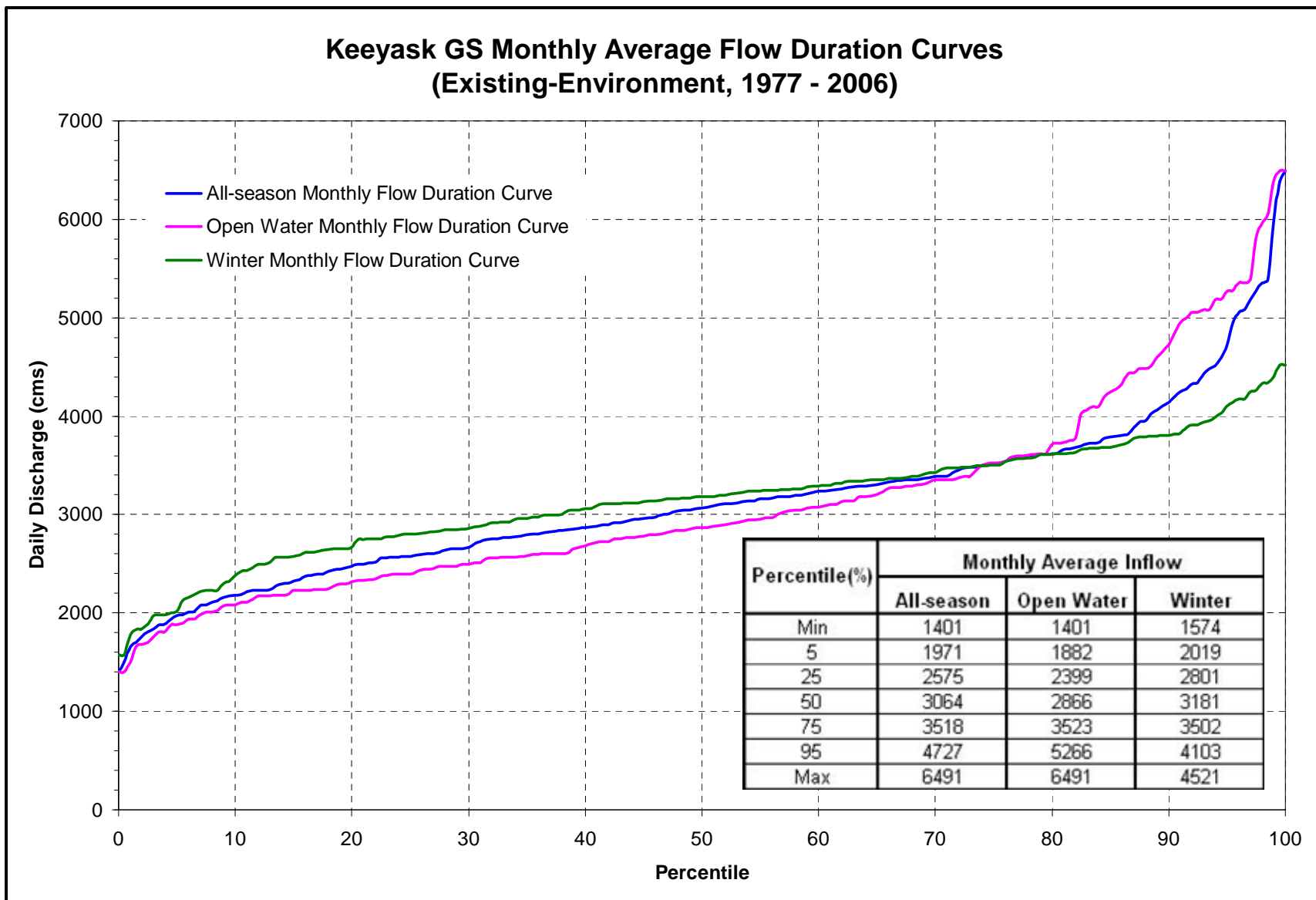


Figure 8 Keyask GS existing environment monthly average inflow duration curves (1977 – 2006)

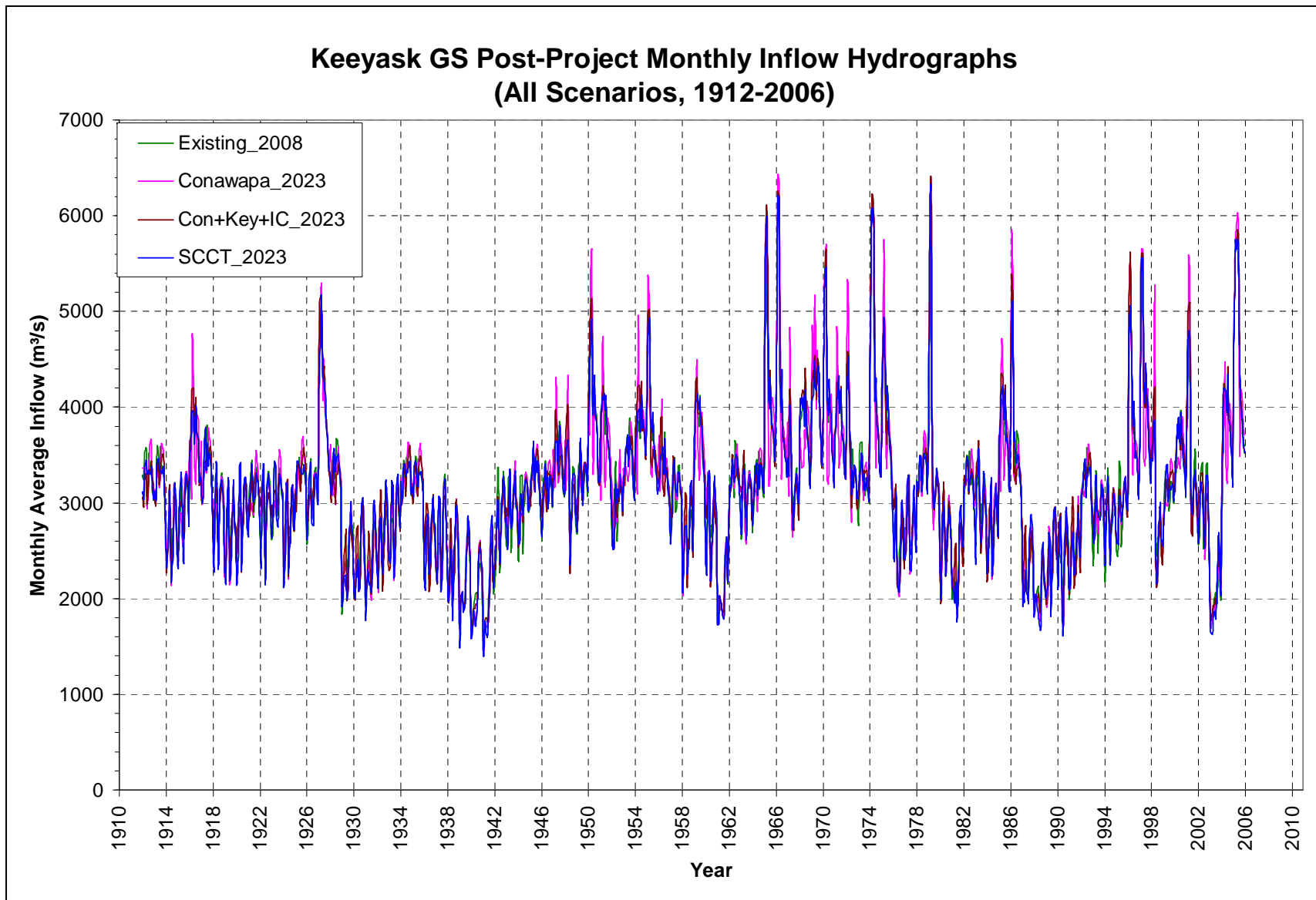


Figure 9 Keyask GS Post-Project inflow hydrographs (1912 – 2006)

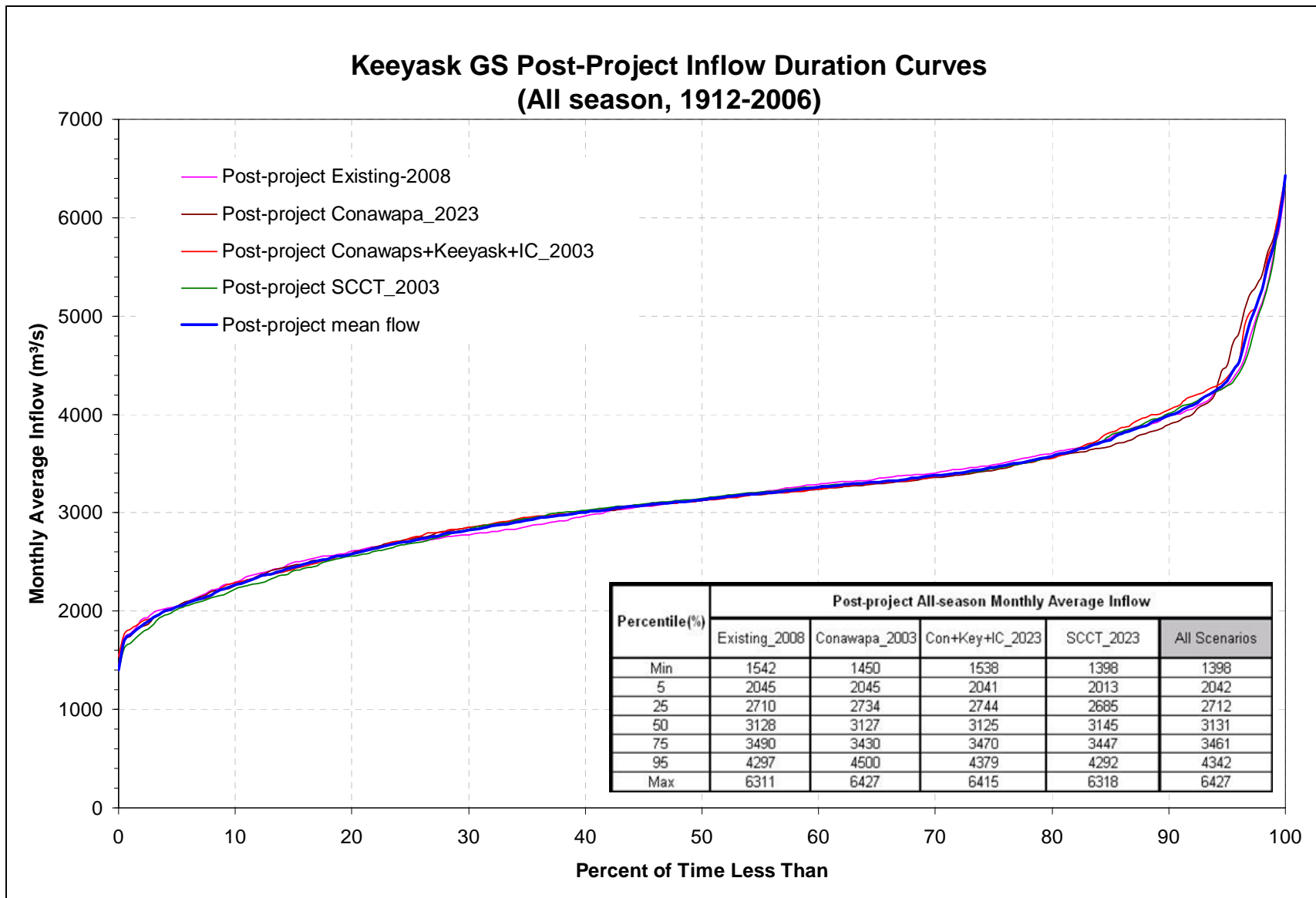


Figure 10 Post-Project all-season inflow duration curves (1912 – 2006)

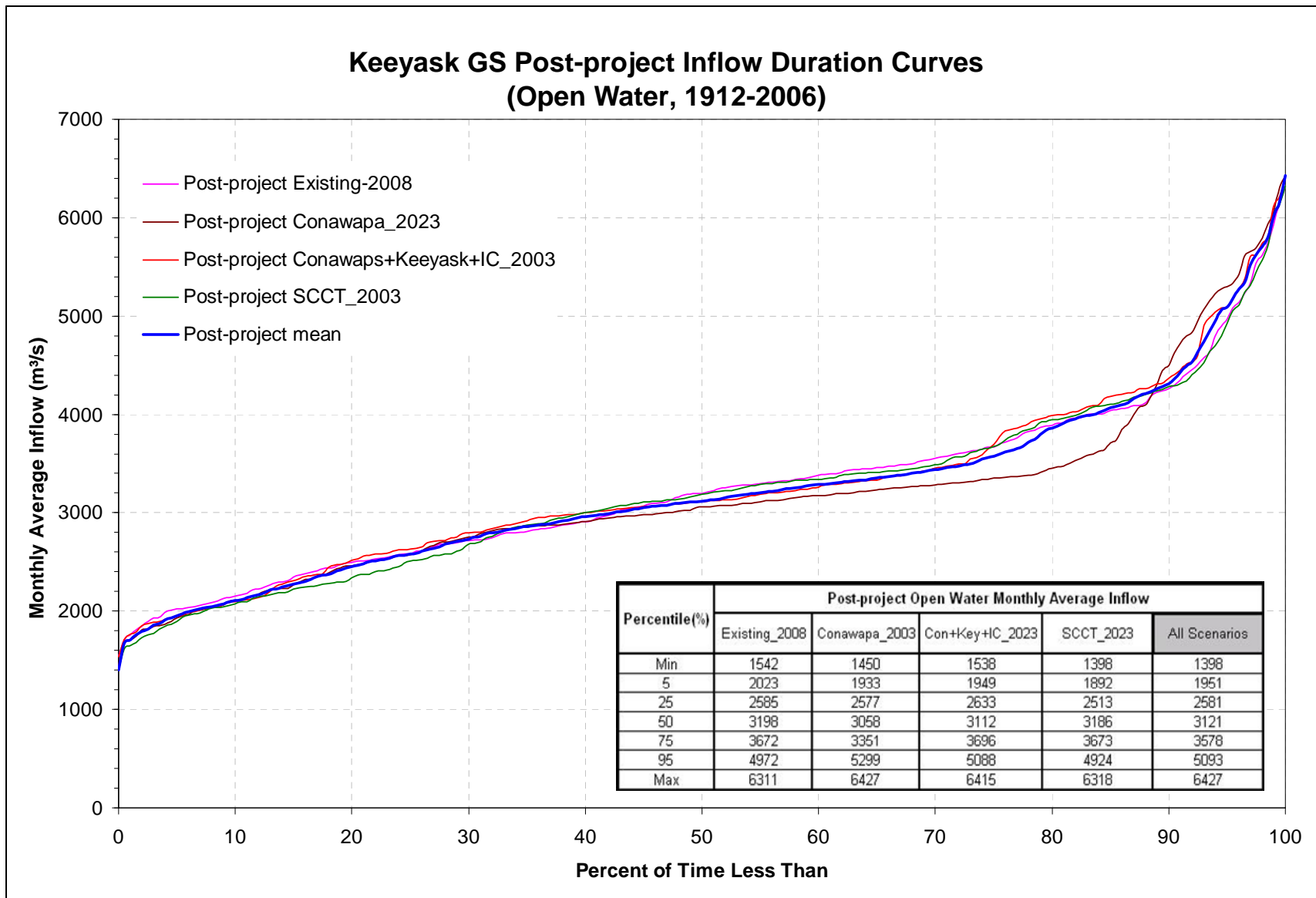


Figure 11 Post-Project open water inflow duration curves (1912 – 2006)

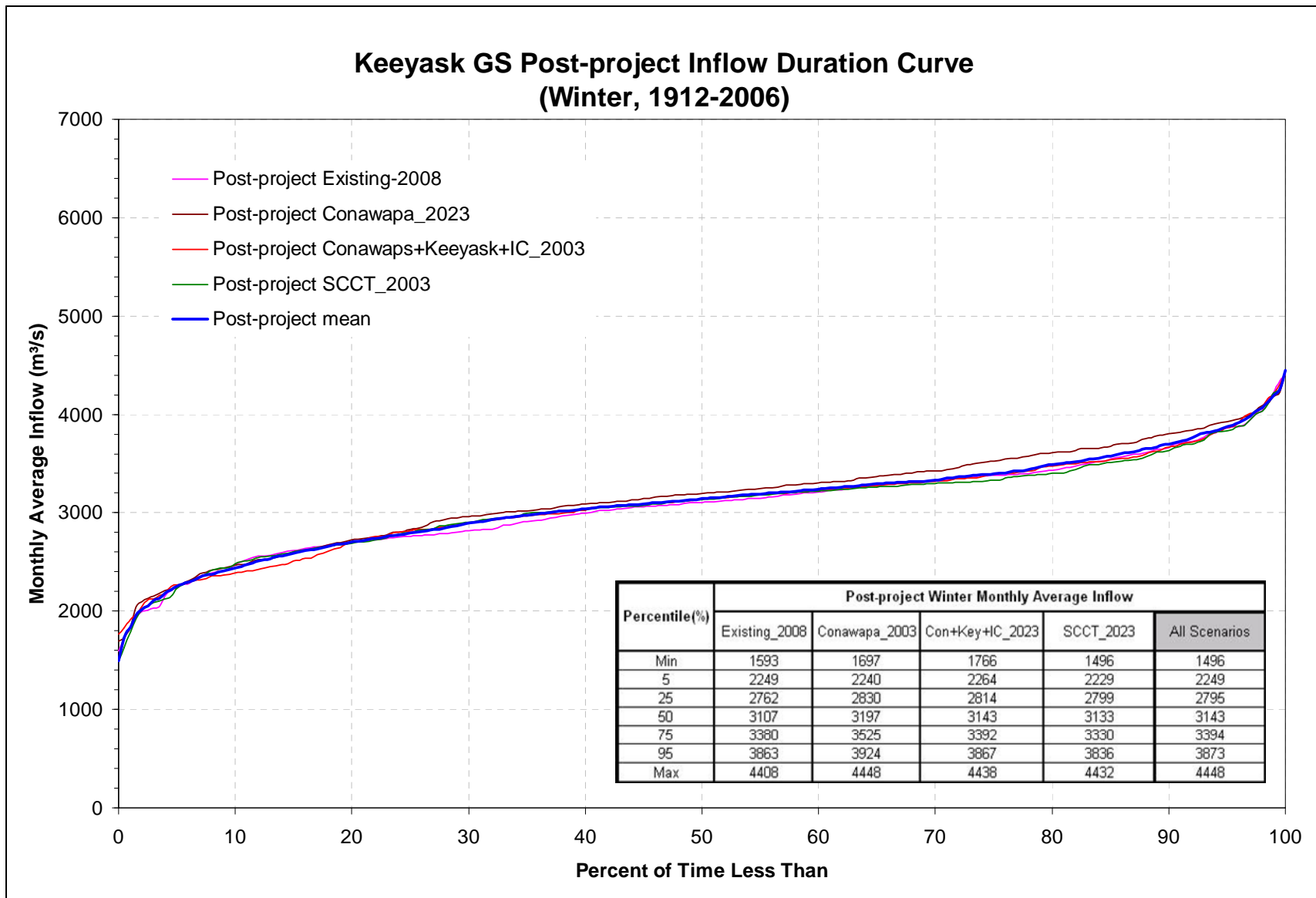


Figure 12 Post-project winter inflow duration curves (1912 – 2006)

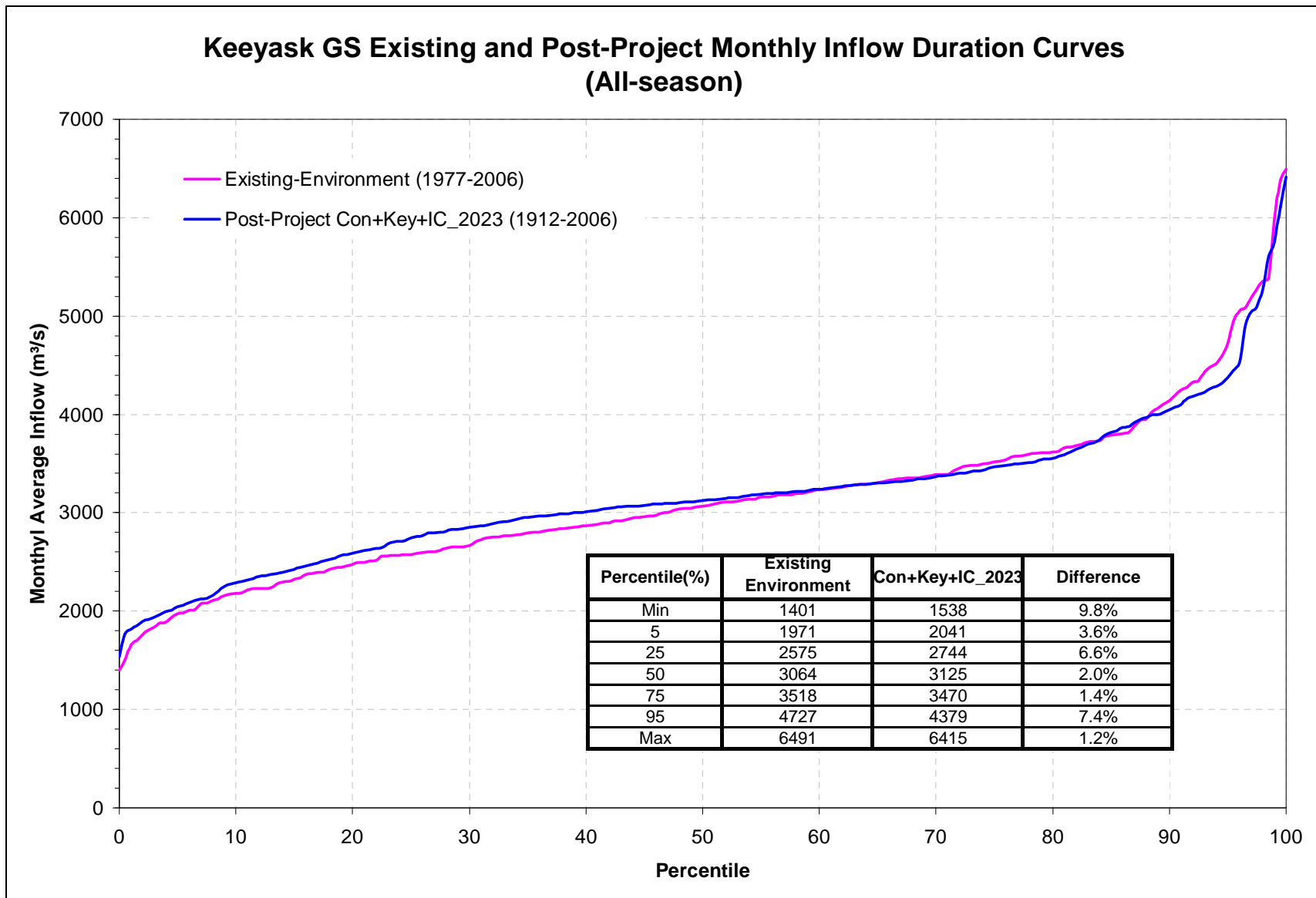


Figure 13 Existing and Post-project all-season inflow duration curves comparison

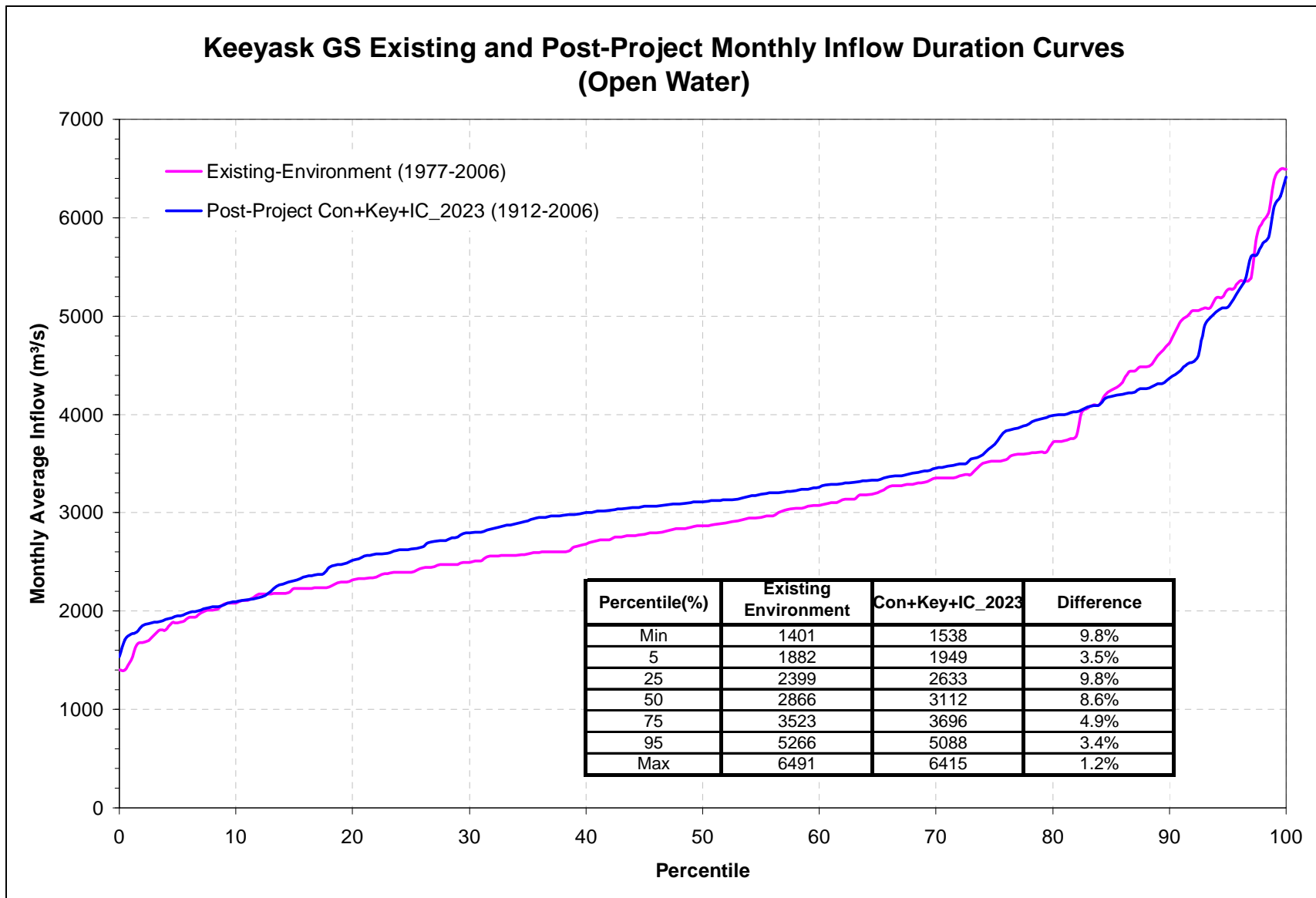


Figure 14 Existing and Post-project open water inflow duration curves comparison

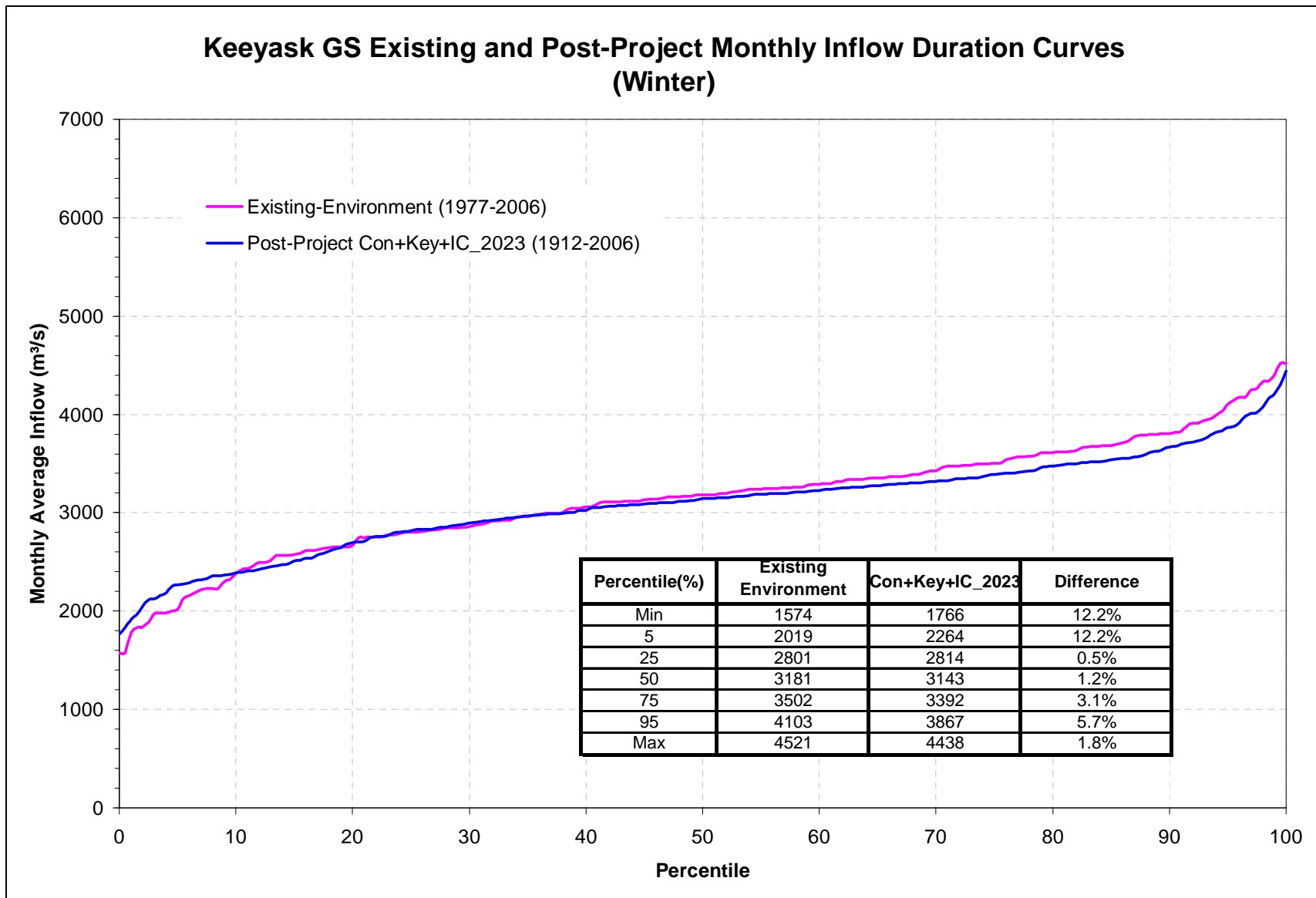


Figure 15 Existing and Post-project winter inflow duration curves comparison

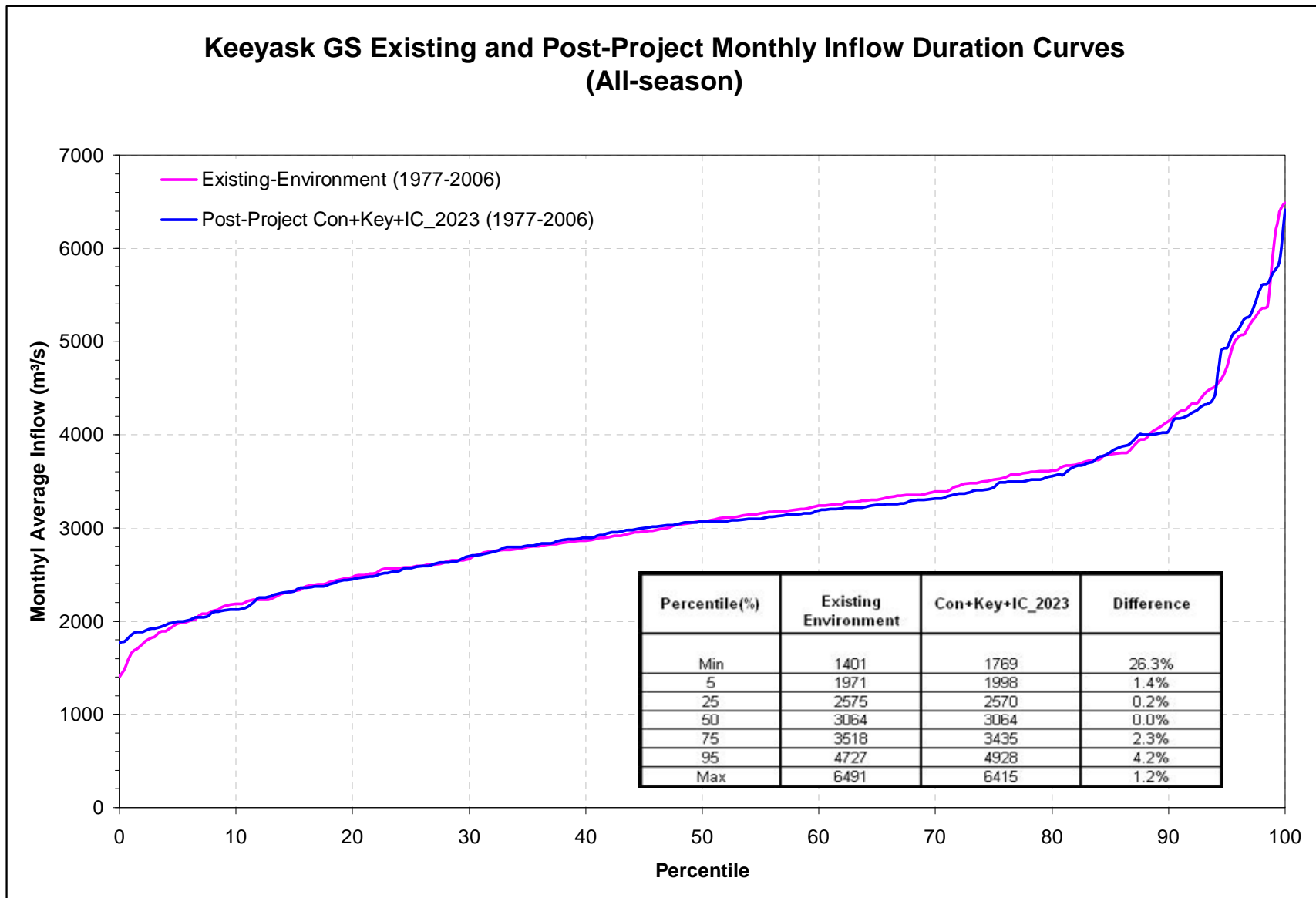


Figure 16 Existing and Post-project all-season inflow duration curves comparison

Table 1 Post-project inflow data (m³/s) for the Keyyask GS under scenario of Conawapa + Keyyask + IC_2023

Year	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Annual
1912				3055	2955	3193	3306	3212	2987	3294	3308	3401	3190
1913	3440	3312	3150	3090	2966	3160	3429	3404	3187	3415	3427	3497	3290
1914	3509	3282	3133	2280	2350	2619	3050	3176	2276	2477	2757	3000	2826
1915	3083	2903	2683	2386	2769	2955	2968	3020	2875	2624	3055	3262	2882
1916	3251	3097	2982	3478	3798	4160	4196	4202	3835	4099	3809	3714	3719
1917	3618	3186	3237	3094	3000	3121	3416	3436	3332	3348	3484	3544	3318
1918	3581	3416	3211	2474	2794	3000	3112	3205	2424	2653	2890	3191	2996
1919	3233	3051	2860	2294	2317	2562	3097	3150	2381	2469	2744	3002	2763
1920	3074	2853	2697	2381	2605	2940	3035	3140	2295	2639	2839	3169	2806
1921	3216	2988	2907	2975	2828	3003	3278	3384	2917	3131	3309	3305	3103
1922	3268	3226	3131	2981	2957	3113	3292	3127	2233	2567	2847	3104	2987
1923	3100	2957	2865	2976	2801	2983	3132	3106	2902	3125	3308	3288	3045
1924	3225	3155	3093	2332	2325	2559	3174	3242	2247	2637	2575	2918	2790
1925	3114	2878	2713	3124	2906	3294	3424	3399	3125	3335	3392	3540	3187
1926	3578	3399	3203	2873	2803	3007	3092	3147	2918	3067	3258	3253	3133
1927	3302	3234	3045	4047	5060	5167	5088	4318	4265	4423	4016	3817	4148
1928	3606	3327	3325	3172	3010	3452	3485	3296	2992	3289	3296	3400	3304
1929	3406	3284	3149	1964	2045	2373	2622	2715	1992	2112	2417	2760	2570
1930	2830	2692	2401	2130	1998	2475	2711	2751	2078	2129	2407	2845	2454
1931	2965	2588	2500	2069	2030	2288	2702	2672	2141	2041	2361	2634	2416
1932	2810	2665	2478	2284	2344	2610	3138	3126	2109	2371	2421	2935	2608
1933	3082	2849	2478	2290	2330	2780	3134	3179	2352	2637	2927	3102	2762
1934	3162	3006	2701	3196	2980	3114	3411	3385	3072	3310	3364	3516	3185
1935	3594	3343	3214	2998	3063	3225	3435	3386	3073	3299	3392	3491	3293
1936	3467	3286	3187	2509	2640	2994	2984	2755	2089	2202	2426	2980	2793
1937	3087	2832	2517	2358	2169	2813	2970	3004	2306	2446	2761	3004	2689
1938	3077	2930	2699	2024	1961	2459	2838	2516	1992	2116	2374	2921	2492
1939	3036	2793	2393	1853	1892	2007	2065	1913	1929	2059	2359	2618	2243
1940	2739	2512	2320	1818	1690	1857	1895	1898	1949	1930	2264	2452	2110
1941	2584	2453	2249	1852	1538	1758	1802	1787	1707	1790	2162	2374	2005
1942	2582	2342	2107	2424	2305	2610	3054	2887	2361	2586	2759	3088	2592
1943	3212	2931	2831	2949	2867	2965	3205	3016	2750	2855	2973	3155	2976
1944	3284	3126	2834	2535	2566	2959	2984	3024	2799	3062	3193	3259	2969
1945	3217	3091	2956	3066	2973	3361	3412	3392	3111	3400	3552	3521	3254
1946	3484	3190	3056	2902	2815	2965	3193	3345	2906	3329	3299	3299	3149
1947	3290	3247	3093	3295	3371	3937	3971	3589	3292	3311	3480	3498	3448
1948	3498	3303	3200	3472	3661	4020	4028	3089	2273	2693	2911	3167	3276
1949	3198	2988	2872	2982	2806	3055	3374	3480	3037	3177	3322	3425	3143
1950	3400	3374	3306	3921	4758	4981	5120	4313	3989	4203	3971	3828	4097
1951	3569	3236	3183	3429	3844	4017	4221	4031	3977	3961	3737	3626	3736
1952	3509	3351	3194	2813	2513	2528	3000	3073	2851	3084	3011	3225	3012
1953	3208	3104	2866	3114	3248	3450	3624	3579	3502	3696	3580	3692	3389
1954	3541	3344	3169	3677	3958	4182	4219	4228	3952	4264	3758	3832	3844
1955	3657	3510	3459	4307	4989	5024	4600	3457	3372	3555	3470	3547	3912
1956	3470	3323	3214	3295	3461	3875	3904	3262	3077	3132	3273	3361	3387
1957	3306	3120	3022	2990	2841	2974	3476	3334	3166	3112	3114	3257	3143
1958	3281	3143	2971	2117	2288	2623	3109	3049	2126	2604	2523	2940	2731
1959	3071	2761	2463	3551	3872	4242	4303	3937	3928	3950	3942	3817	3653
1960	3573	3347	3209	2915	2834	3086	3336	3141	2135	2575	2586	2951	2974
1961	3023	2808	2703	1766	1744	2020	1981	1938	1848	1866	2238	2413	2196
1962	2538	2331	2179	3106	3067	3238	3502	3355	3287	3251	3289	3481	3052
1963	3433	3260	3171	3151	3049	3271	3548	3054	2825	2806	3149	3151	3156
1964	3237	3080	2819	2966	3050	3123	3238	3316	3082	3361	3386	3417	3173
1965	3411	3352	3226	4069	5479	6110	5937	4338	4075	4379	3776	3789	4328
1966	3671	3509	3394	4245	5344	6249	6170	4531	4005	4069	3711	3649	4379
1967	3536	3381	3266	3473	3478	4187	3556	3112	2745	2707	3027	3191	3305
1968	3269	3121	2835	3603	4090	4072	4182	4155	3998	4405	3874	3757	3780
1969	3554	3320	3199	4163	4292	4379	4472	4530	4081	4503	4438	4224	4096
1970	3867	3516	3379	4129	5088	5340	5619	4083	3989	4044	3998	3887	4245
1971	3627	3349	3181	3647	3882	4258	4263	4123	3998	4205	3718	3723	3831
1972	3552	3315	3251	4174	4585	4510	3830	3211	2944	3173	3196	3327	3589
1973	3279	3068	2940	3071	3091	3233	3466	3488	3156	3334	3316	3345	3232
1974	3336	3199	3147	4203	5743	6223	6131	5801	4568	4093	3873	3733	4504
1975	3546	3350	3276	4078	4370	4929	4776	3843	3614	3848	3714	3735	3923
1976	3527	3337	3170	2933	2971	3194	2866	2145	2091	2067	2412	2767	2790
1977	2896	2481	2310	2538	2579	2734	3241	3285	2516	2462	2616	2968	2719
1978	3057	2830	2638	3131	3069	3220	3498	3489	3127	3499	3513	3499	3214
1979	3568	3410	3247	4021	5274	6415	5244	3227	2946	2926	3155	3196	3886
1980	3242	3069	2855	1959	2105	2716	3211	3015	2256	2443	2398	2896	2680
1981	3010	2760	2446	2123	2087	2156	2485	2570	1913	2036	2365	2678	2386
1982	2799	2570	2359	3160	3287	3202	3482	3307	3094	3224	3272	3353	3092
1983	3253	3120	3025	3164	3369	3498	3643	3252	2486	2591	2829	3089	3110
1984	3064	2920	2700	2180	2358	2881	3041	3212	2481	2627	2868	3006	2778
1985	3069	2921	2645	3498	4018	4317	4354	4264	3998	4224	3694	3707	3726
1986	3517	3253	3148	4119	5380	5069	3318	3378	3196	3324	3370	3405	3706
1987	3414	3245	3129	2005	2105	2591	2744	2119	2009	1998	2316	2469	2512
1988	2703	2395	2322	1918	2042	2043	1989	2050	1984	1850	2127	2310	2144
1989	2448	2293	2132	1957	1938	2473	2541	2569	1883	2091	2376	2894	2300
1990	2961	2636	2410	2530	2797	2790	2887	2353	1783	1870	2315	2542	2490
1991	2805	2412	2252	2041	2369	2631	3064	2720	2120	2306	2264	2784	2481
1992	2978	2724	2268	2999	3041	3204	3252	3302	3065	3366	3316	3487	3084
1993	3518	3302	3080	2829	2579	3026	3031	3035	2852	2876	2820	2992	2995
1994	3061	3143	3095	2436	2637	2893	3098	3065	2377	2633	2814	2986	2853
1995	3151	2907	2793	2591	2584	2703	3133	3076	2952	2978	2998	3148	2918
1996	3217	3079	2874	3629	4928	5622	5131	3998	3758	3849	3498	3540	3927
1997	3405	3188	3057	3888	5175	5604	5609	4282	3998	4260	4005	3984	4205
1998	3737	3435	3272	3518	3664	4039	4199	2794	2124	2203	2462	2945	3200
1999	2836	2511	2357	2798	2859	3020	3248	3067	3019	3091	3318	3294	2952
2000	3340	3260	3144	3116	3426	3802	3864	3890	3557	3773	3548	3665	3532
2001	3569	3399	3201	3691	4902	5042	5087	3562	2706	2654	3058	3242	3676
2002	3215	3069	2811	3106	3110	3220	3303	3311	3094	2532	2613	2956	3028
2003	3097	2875	2757	1833	1769	1887	1921	1907	1999	1949	2273	2377	2220
2004													

Table 2 - Existing environment flow data (cms) for the Keyask GS

Year	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Annual
1977									2083	2236	2809	2881	
1978	2820	2804	2997	2625	2331	2231	2271	2375	2455	3352	3663	3625	2796
1979	3574	3633	3586	3228	4026	5266	5277	4201	2574	2866	3481	3364	3759
1980	3159	3111	3316	3181	2510	2077	1981	2108	2494	2869	3185	3169	2762
1981	3183	3298	2959	1971	2228	2007	2448	2113	2293	2569	3140	2995	2597
1982	2564	2570	2461	2380	3184	2474	2378	2607	2964	3523	3551	3484	2847
1983	3355	3258	3119	3166	3180	3041	2829	2888	2914	3191	3497	3286	3143
1984	3340	3252	3319	3216	2949	2914	2797	2670	2599	2855	3039	3245	3016
1985	3144	3246	2918	2950	3356	3104	3268	2969	3049	3311	3463	3569	3196
1986	3787	3794	3677	3340	4946	5191	4444	3229	3134	3292	3389	3686	3827
1987	3607	3425	3365	3212	3021	2420	2399	2228	2344	2475	2791	2873	2844
1988	2750	2745	2575	2019	2769	2176	1756	1683	1700	1895	2227	2303	2216
1989	2229	2186	2122	2004	2398	1882	2026	2398	2605	2723	2756	2861	2351
1990	2915	2772	2569	2159	2566	2550	2246	2176	2437	2767	2898	2826	2572
1991	2647	2493	2325	2213	2497	2136	2183	2235	2190	2473	2652	2590	2386
1992	2751	2777	2616	2422	2755	2595	2317	2336	2507	3715	3816	3353	2830
1993	3351	3569	3280	2518	2074	1656	1809	2606	4097	3596	2960	3478	2912
1994	3614	3426	3107	2801	3064	2594	2716	2706	2655	2892	3063	3088	2976
1995	3349	3238	3134	3117	3002	2837	2556	2954	3103	3391	3200	3111	3082
1996	3159	3059	3049	2974	3518	4657	5082	4597	3291	3585	3408	3729	3680
1997	3609	3666	3777	3807	4481	5381	5357	4840	3731	3594	3884	4029	4184
1998	3992	3955	3710	3694	3774	4063	4246	3726	2882	2842	2854	2829	3546
1999	2846	2925	2654	2664	2582	2775	2756	2680	2784	3078	3114	3162	2834
2000	3300	3495	3391	3242	3072	2801	3376	3500	3617	3753	3680	3540	3397
2001	3793	3943	3804	3498	4433	4727	4998	4329	3605	3542	3477	3378	3962
2002	3502	3194	3000	2656	2817	3092	3141	3333	3276	3204	3046	3247	3126
2003	3253	2978	2844	2431	2294	1941	1938	1878	1499	1401	1574	1828	2151
2004	1834	1890	1980	1781	2178	2929	3451	3351	3300	3608	3829	3618	2816
2005	3909	4265	4103	4331	5058	5804	6046	6388	6491	5961	4400	4143	5080
2006	4179	4249	4340	4521	5084	5183	4515	4275	3392	2562	2635	3289	4018
Mean	3225	3214	3107	2901	3177	3190	3193	3082	2936	3104	3183	3219	3114
Min	1834	1890	1980	1781	2074	1656	1756	1683	1499	1401	1574	1828	2151
Max	4179	4265	4340	4521	5084	5804	6046	6388	6491	5961	4400	4143	5080